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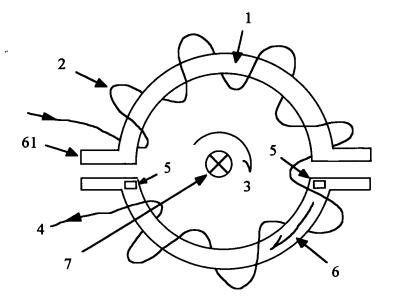


Fig. 1: A clamp-on sensor

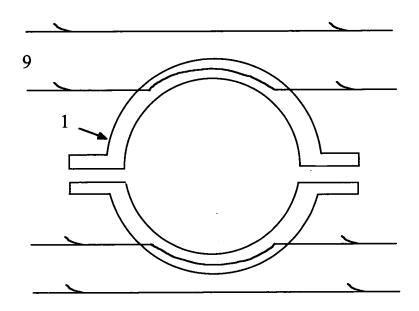


Fig. 2: Uniform magnetic field (H_u) 9 of the earth H_e acting on the core.

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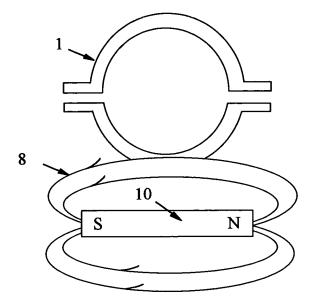
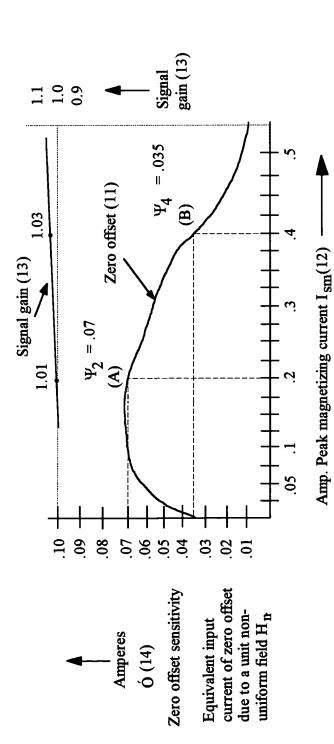


Fig. 3: A non-uniform magnetic field (H_n) 8 from a magnet acting on the core.

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Normalized Signal Gain (g) vs. I_{sm} and
Normalized Zero Offset from H_n vs. I_{sm} for
Five inch diameter aperture sensor #88.

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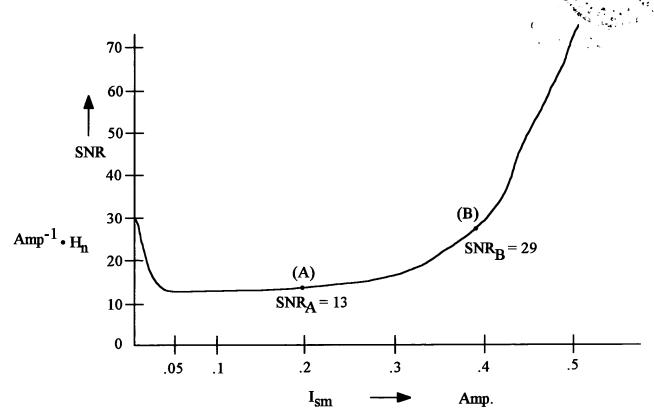
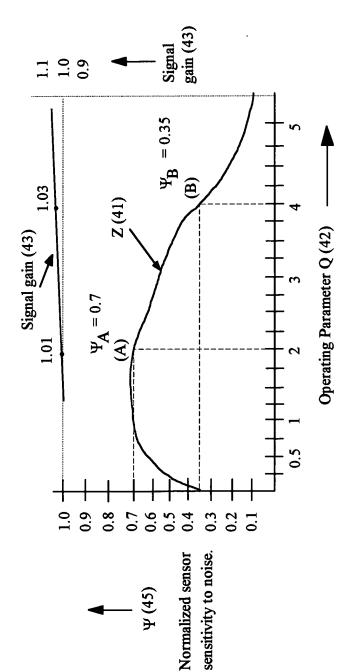


Figure 5 Signal to Noise Ratio (SNR) for Non-Uniform Field H $_{n}$ vs. Operating Parameter I $_{sm}$ for

5" dia. aperture clip #88 in SN 2336

SNR =
$$\frac{\delta V_{\delta I}}{\delta V_{\delta N}}$$
 input input input $\frac{\delta V_{\delta N}}{\delta N}$ output $\frac{Z}{g}$ = equivalent input offset I per unit non-uniform field H_n

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Normalized Signal Gain vs. Operating Parameter Magnitude and Normalized Sensitivity to H_n vs. Operating Parameter Magnitude for A Hypothetical Sensor Presented as an Illustration.

Fig. 6

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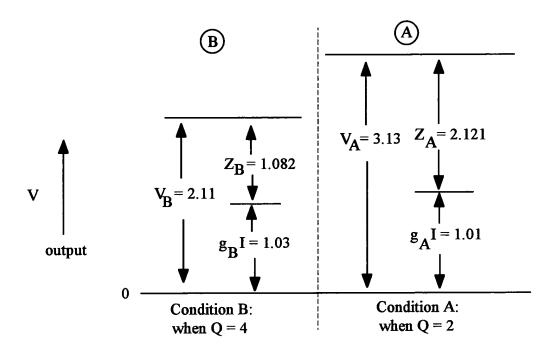


Fig. 7
The illustration displays typical relationships between error, gain, etc., before correction of a hypothetical sensor.

Variables:

I = 1

N = 3

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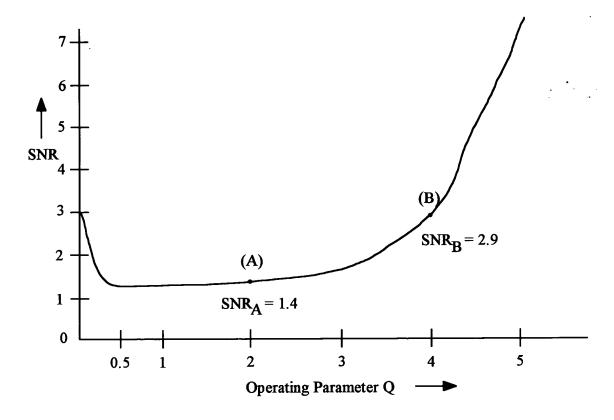


Figure 8
Signal to Noise Ratio (SNR)
vs.
Operating Parameter Q
for

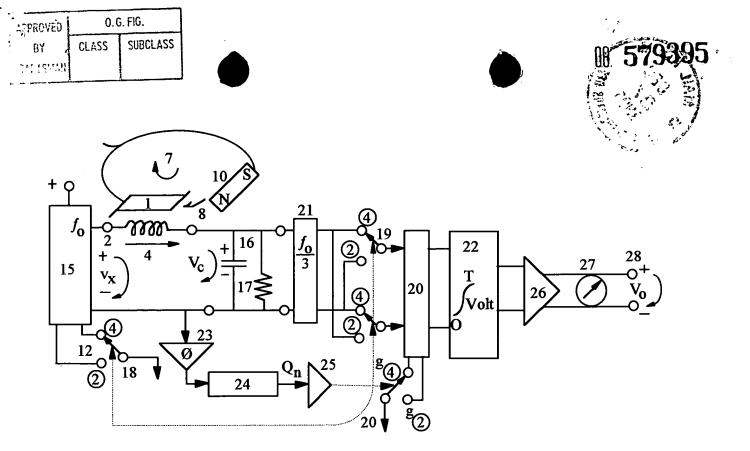


Fig. 9: A switching implementation of the mathematical relationship shown in Eq. i).

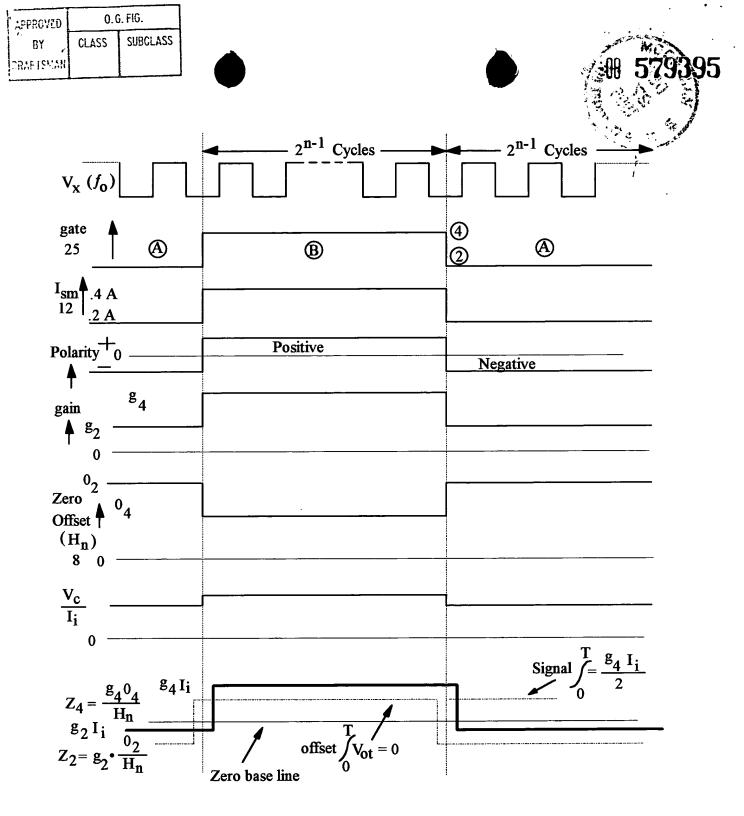


Fig. 10: Voltages in Fig. 9 shown as they change from time interval (18).

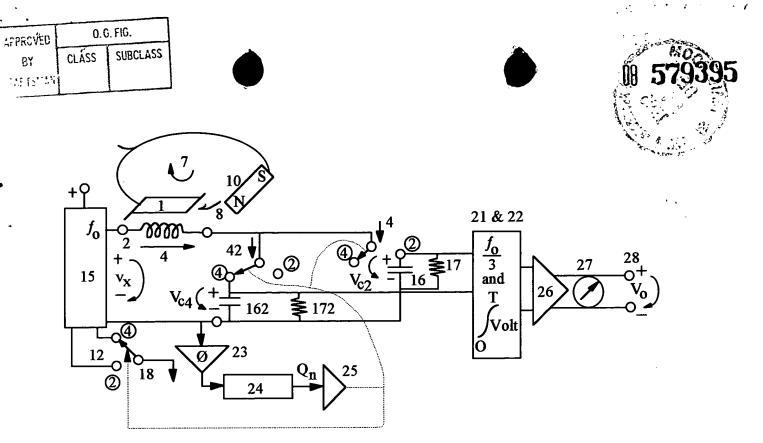


Fig. 11: A simpler implementation of the method defined in Eq. i).

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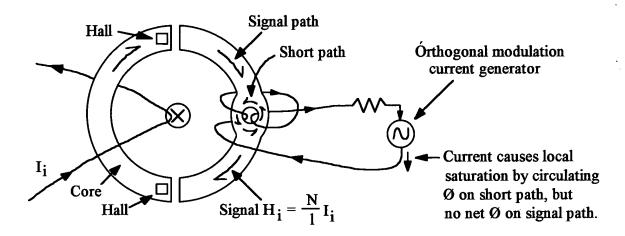


Fig. 12: Proposed core structure and magnetic reluctance selective modulation means for a Hall type clamp-on DC ammeter.

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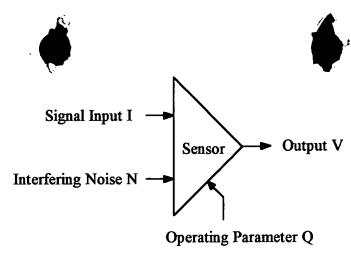




Fig. 13. General representation of a Sensor described in Eq. a) thru Eq. j).